


PROJECT :			DATE :	3/4/2011
PROJ. NO.:			BY :	S.R
CLIENT :			REV :	A
UNIT :			DOC NO.:	0

Tube Rupture Relief Rate Calculation (Two Phase - based on API 520 section D.2.1 A1)

Input Data		
HP Side Vapor Mass fraction	----	0.1000
HP Side Vapor Mass Density	lb/ft3	1.33
HP Side Liquid Mass Density	lb/ft3	49.54
HP Side Latent Heat of Vaporization (hvl)	btu/lb	728.3
HP Side Liquid Specific Heat	btu/lbR	1.17
HP Side Operating Pressure	psig	600.00
LP Side PSV Set Pressure	psig	200.00
HP Side Operating Temperature	R	948.80
Exchanger Tube Length	in	192.00
Exchanger Tube Inside Diameter	in	0.7320

A1:		
$R_{vi} = 1/ R_i - 1/R_v$	lb/ft3	0.7306
$R_o = X_v R_v + (1-X_v) R_i$	lb/ft3	44.7183
HP Side Operating Pressure (Po)	psia	614.70
LP Side Design Pressure (Pb)	psia	214.70
ω (from equation D.1)		8.25
set to zero		0.0011
$\eta_c = P_c/P$		0.834
Critical Pressure (Pc)	psia	512.42
Flow Regime	----	Critical
used Pb	psia	512.42
Tube Discharge Area	in2	0.421
Mass Flux Rate Through Tubesheet (G1)	lb/hr in2	81795.5
Mass Flow Rate Through Tubesheet	lb/hr	34405

Iteration on η_1		0.983
η_2		0.480
delta (set to zero by changing η_1)		-0.4980
friction factor $f = 1/ (44.137 + 11.691 \ln di)$		0.02470
Mass Flow Rate Through Tube (G2)	lb/hr in2	47066.7
Mass Flow Rate Through Tube	lb/hr	19797
Total Flow Rate Through Breakage	lb/hr	54202

General Notes	

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Tube Rupture Relief Rate Calculation (Two Phase - based on API 520 section D.2.1 A2)

Input Data		
HP Side Vapor Mass fraction	---	0.2000
HP Side Vapor Mass Density	lb/ft3	1.33
HP Side Liquid Mass Density	lb/ft3	20.10
HP Side Vapor Mass fraction @ 90% Pop HPS	%	0.9000
HP Side Vapor Mass Density @ 90% Pop HPS	lb/ft3	1.20
HP Side Liquid Mass Density @ 90% Pop HPS	lb/ft3	16.75
HP Side Operating Pressure	psig	66.00
LP Side PSV Set Pressure	psig	15.00
Exchanger Tube Length	in	192.00
Exchanger Tube Inside Diameter	in	0.7320

A2 :		
$R9 = Xv9 Rv + (1-Xv9) Ri$	lb/ft3	2.7550
$Ro = Xv Rv + (1-Xv) Ri$	lb/ft3	16.3464
HP Side Operating Pressure (Po)	psia	80.70
LP Side Design Pressure (Pb)	psia	29.70
ω (from equation D.3)		44.400
set to zero		0.0012
$\eta_c = Pc/P$		0.931
Critical Pressure (Pc)	psia	75.16
Flow Regime	----	Critical
used Pb	psia	75.16
Tube Discharge Area	in2	0.421
Mass Flux Rate Through Tubesheet (G1)	lb/hr in2	8629.7
Mass Flow Rate Through Tubesheet	lb/hr	3630

Iteration on η_1		0.957
η_2		0.919
delta (set to zero by changing η_1)		6.4331
friction factor $f = 1 / (44.137 + 11.691 \ln di)$		0.02470
Mass Flow Rate Through Tube (G2)	lb/hr in2	8513.3
Mass Flow Rate Through Tube	lb/hr	3581
Total Flow Rate Through Breakage	lb/hr	7211

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Tube Rupture Relief Rate Calculation (Two Phase - based on API 520 section D.2.1 A3)

Input Data		
HP Side Vapor Mass fraction	---	0.1000
HP Side Vapor Mass Density	lb/ft3	6.58
HP Side Liquid Mass Density	lb/ft3	61.15
HP Side Vapor Specific Heat Ratio	----	1.00
HP Side Operating Pressure	psig	558.25
LP Side PSV Set Pressure	psig	101.50
Exchanger Tube Length	in	192.00
Exchanger Tube Inside Diameter	in	1.0000

A3 :		
$R_o = X_v R_v + (1-X_v) R_l$	lb/ft3	55.6951
HP Side Operating Pressure (Po)	psia	572.95
LP Side Design Pressure (Pb)	psia	116.20
ω (from equation D.4)		0.85
set to zero		0.0011
$\eta_c = P_c/P$		0.584
Critical Pressure (Pc)	psia	334.84
Flow Regime	----	Critical
used Pb	psia	334.84
Tube Discharge Area	in ²	0.785
Mass Flux Rate Through Tubesheet (G1)	lb/hr in ²	192950.9
Mass Flow Rate Through Tubesheet	lb/hr	151466

Iteration on η_1		0.851
η_2		0.452
delta (set to zero by changing η_1)		3.2214
friction factor $f = 1 / (44.137 + 11.691 \ln di)$		0.02266
Mass Flow Rate Through Tube (G2)	lb/hr in ²	149362.9
Mass Flow Rate Through Tube	lb/hr	117250
Total Flow Rate Through Breakage	lb/hr	268716

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Tube Rupture Relief Rate Calculation (Two Phase - based on API 520 section D.2.2 A1)

Input Data		
HP Side Operating Temperature	R	520.00
HP Side Liquid Saturatin Pressure (Ps)	psia	107.6
HP Side Liquid Mass Density @ Ps	lb/ft3	31.64
HP Side Vapor Mass Density @ Ps	lb/ft3	1.00
HP Side Liquid Mass Density	lb/ft3	31.92
HP Side Latent Heat of Vaporization (hvl) @ Ps	btu/lb	152.3
HP Side Liquid Specific Heat	btu/lbR	0.64
HP Side Operating Pressure	psig	286.00
LP Side PSV Set Pressure	psig	10.00
Exchanger Tube Length	in	192.00
Exchanger Tube Inside Diameter	in	0.7320

A1:		
$R_{vl} = 1/ R_l - 1/R_v$	lb/ft3	0.9684
HP Side Operating Pressure (Po)	psia	300.70
LP Side Design Pressure (Pb)	psia	24.70
ω_s (from equation D.8)	----	8.50
η_{st}	----	0.944
Subcooling Region	----	High Subcooling
$\eta_s = P_s/P_o$	----	0.36
η_c from Figure D3 (for low subcooling only)	----	0.300
Critical Pressure (Pc)	psia	90.21
Flow Regime	----	Critical
used η as per type of flow regime	----	0.30
used P as per type of flow regime	psia	107.600
Mass Flux Rate Through Tubesheet (G1)	lb/hr in2	189012
Tube Discharge Area	in2	0.421
Mass Flow Rate Through Tubesheet	lb/hr	79502

Iteration on η_1		0.983
η_2		0.491
delta (set to zero by changing η_1)		-0.0422
friction factor $f = 1 / (44.137 + 11.691 \ln di)$		0.02470
Mass Flow Rate Through Tube (G2)	lb/hr in2	28060
Mass Flow Rate Through Tube	lb/hr	11803
Total Flow Rate Throubh Breakage	lb/hr	91305

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Tube Rupture Relief Rate Calculation (Two Phase - based on API 520 section D.2.2 A2)

Input Data		
HP Side Operating Temperature	R	600.00
HP Side Liquid Saturatin Pressure (Ps)	psia	171.80
HP Side Vapor Mass fraction @ 90% Ps	---	0.1050
HP Side Liquid Mass Density @ 90% Ps	lb/ft3	33.18
HP Side Vapor Mass Density @ 90% Ps	lb/ft3	1.65
HP Side Liquid Mass Density	lb/ft3	32.74
HP Side Operating Pressure	psig	286.00
LP Side PSV Set Pressure	psig	10.00
Exchanger Tube Length	in	192.00
Exchanger Tube Inside Diameter	in	0.7320

A1:		
$R9 = Xv9 Rv9 + (1 - Xv9) Rl9$	lb/ft3	29.8719
HP Side Operating Pressure (Po)	psia	300.70
LP Side Design Pressure (Pb)	psia	24.70
ω_s (from equation D.9)		0.86
η_{st}		0.633
Subcooling Region		High Subcooling
$\eta_s = Ps/Po$		0.57
η_c from Figure D3 (for low subcooling only)		0.300
Critical Pressure (Pc)	psia	90.21
Flow Regime	----	Critical
used η as per type of flow regime		0.30
used P as per type of flow regime	psia	171.800
Mass Flux Rate Through Tubesheet (G1)	lb/hr in2	156398
Tube Discharge Area	in2	0.421
Mass Flow Rate Through Tubesheet	lb/hr	65785

Iteration on η_1		0.947
η_2		0.292
delta (set to zero by changing η_1)		0.0412
friction factor $f = 1 / (44.137 + 11.691 \ln di)$		0.02470
Mass Flow Rate Through Tube (G2)	lb/hr in2	53002
Mass Flow Rate Through Tube	lb/hr	22294
Total Flow Rate Throuh Breakage	lb/hr	88078

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